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G. Robert Brakenridge, Sagy Cohen, Albert J. Kettner, Tom De Groeve, Son V. Nghiem, James P.M. Syvitski, Balazs M. Fekete

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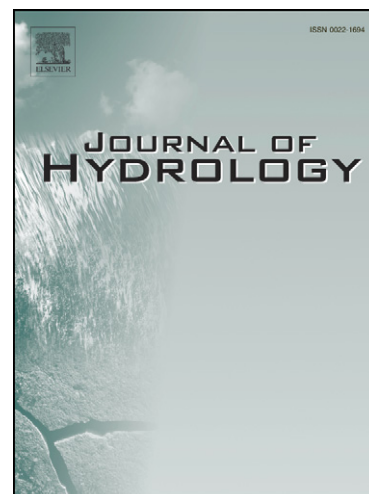
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1 **Calibration of Satellite Measurements of River Discharge Using a**
2 **Global Hydrology Model**

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4 G. Robert Brakenridge¹, Sagy Cohen^{1,2}, Albert J. Kettner¹, Tom De Groeve³, Son V.
5 Nghiem⁴, James P.M. Syvitski¹, and Balazs M. Fekete⁵

6
7 ¹Community Surface Dynamics Modeling System, Institute of Arctic and Alpine
8 Research, University of Colorado, Boulder, Colorado 80309, USA

9
10 ²Department of Geography, University of Alabama, Box 870322, Tuscaloosa, AL
11 35487, USA

12
13 ³Joint Research Centre, European Commission, Ispra, Italy

14 ⁴Jet Propulsion Laboratory, California Institute of Technology
15 Pasadena, California, 91109, USA

16
17 ⁵CUNY Environmental CrossRoads Initiative, NOAA-CREST Center, The City College
18 of New York, City University of New York, New York, New York, 10031, USA

19
20 Email contact corresponding author: Robert.Brakenridge@Colorado.edu

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22 Water Balance Model

23

24

Abstract

25 Measurements of river discharge and watershed runoff are essential to water
26 resources management, efficient hydropower generation, accurate flood prediction and
27 control, and improved understanding of the global water cycle. Previous work
28 demonstrates that orbital remote sensing can measure river discharge variation in a
29 manner closely analogous to its measurement at ground stations, and using reach flow
30 surface area instead of stage as the discharge estimator. For international measurements,
31 hydrological modeling can, in principle, be used to provide the needed calibration of
32 sensor data to discharge. The present study tests this approach and investigates the
33 accuracy of the results. We analyze 6 sites within the U.S. where gauging station, satellite
34 measurements, and WBM model results are all available. Knowledge is thereby gained
35 concerning how accurately satellite sensors can measure discharge, if the signal is
36 calibrated only from global modeling results without any ground-based information. The
37 calibration (rating) equations obtained for the remote sensing signal are similar, whether
38 based on gauging station or on model information: r^2 correlation coefficients for least
39 squares fits at one example site (#524; White River, Indiana) are both .66 ($n = 144$,
40 comparing monthly daily maxima, minima, and mean, 2003-2006). Space-based 4-day
41 mean discharge values for this site when using the model calibration are accurate to
42 within +/- 67% on the average ($n = 1824$; largest percent errors occur at low discharges),
43 and annual total runoff is accurate to +/- 9 %, 2003-2008. Comparison of gauging station
44 versus modeled discharge commonly indicates a small positive model bias; the observed
45 errors of satellite-observed annual runoff are also positive and could be improved by bias
46 removal from the rating curves. Also, analysis of a large flood event, along the Indus
47 River in 2010, shows that the model does not capture flood wave attenuation by overbank
48 flow, and thus predicts faster flood wave celerity and higher peak discharge than was
49 measured by the remote sensing. The incorporation of overbank processes would improve
50 discharge estimation via modeling, and also facilitate more accurate satellite-based
51 measurement of peak discharge. The analysis shows that existing and planned microwave
52 sensors can usefully characterize global river discharge dynamics, and that water balance
53 model-based rating curves provide acceptable calibration of remote sensing signal to
54 discharge.

55 **1. Introduction**

56 Measurements of river discharge and watershed runoff are essential to water
57 resources management, efficient hydropower generation, accurate flood prediction
58 and control, and improved understanding of the global water cycle. River discharge
59 at-a-site is an integrated signal of water cycle processes over the catchment area
60 upstream, and large amounts of variability over relatively small amounts of time
61 commonly occur. This makes high frequency (daily) measurements necessary for
62 many rivers (Fekete et al., 2012). Major efforts have been made to improve the
63 international availability of ground-based discharge data, but many nations do not
64 share hydrological data, and the network of ground stations on a global basis is
65 inadequate. Rivers and tributary streams transgress political borders, causing
66 downstream nations to experience severe constraints in predicting surface water
67 incoming from upstream. Global hydrological modeling can assist in evaluating
68 runoff (Littlewood et al., 2003; Sivapalan et al., 2003); such modeling is
69 complementary to direct measurements, but not an accurate substitute for them
70 (e.g. Cohen et al., 2011).

71 Space-based observational approaches for direct, sustained characterization
72 of river discharge and runoff have so far been little utilized. Yet, they are now
73 feasible, using existing and planned sensors. New processing techniques using
74 frequent-revisit microwave-frequency sensing (Brakenridge et al., 2007) have
75 demonstrated a capability to track discharge changes via the sensitive response to
76 water surface area changes. Such information can be obtained globally and in “near
77 real time” (within several hours after satellite overpass). These data require some

78 method of calibration to discharge to be most useful. Here we employ a global water
79 balance runoff model (WBM; Wisser et al., 2010; Wisser et al., 2008) to calibrate
80 remote sensing to discharge: at measurement sites within the U.S. that are
81 coincident to comparison ground gaging stations. Error analysis indicates that
82 model-based calibration of the remote sensing signal can substitute for calibration
83 by ground-based discharge data at many sites without significant loss of discharge
84 accuracy. However, along some major rivers (the study example is the Indus, in
85 Pakistan), WBM does not presently account for very significant flood wave
86 attenuation via overbank flooding. Peak discharge downstream is thus over-
87 estimated, and model improvements would facilitate more accurate rating curves.

88 **2. Measuring Discharge and Runoff From Space**

89 Previous work demonstrates that orbital remote sensing from a variety of
90 sensors has the capability to characterize river discharge variation in a manner
91 closely analogous to its measurement at ground stations (Brakenridge et al., 2005;
92 Brakenridge et al., 2007; Khan et al., 2011; Smith, 1997; Smith et al., 1996; Temimi,
93 2011). Thus, for ground gauging stations, frequent or continuous river stage heights
94 are calibrated to discharge using infrequent, current meter traverses. These
95 intermittent (“actual discharge”) measurements obtained in the field sample flow
96 velocities and channel cross sectional areas under varying flow conditions, as stage
97 values are recorded. Empirical, “rating curves” that compare stage to discharge are
98 thereby developed. Conventional ground-based discharge values based on stage-
99 discharge rating curves have an accuracy of 5 to 10% (Hirsch and Costa, 2004; Olson
100 and Norris, 2007; Rantz et al. 1982; Schmidt, 2003).

101 In comparison, and for measurement via orbital remote sensing methods,
102 consider the flow continuity equation:

$$103 \quad Q = wdu \quad (1)$$

104 where Q is discharge in m^3/sec , w is flow width (m), d is flow depth (m), and u is
105 flow velocity (m/sec). Inherent to flow continuity is that measurements which
106 monitor flow width also provide a proxy indicator of changing discharge (unless the
107 channel banks are vertical). Along most rivers, w is similar to d in its sensitivity to
108 discharge change (Bjerklie et al., 2004); both are more robust predictors of
109 discharge than u . Thus, w measurements can be transformed, via a rating curve, to
110 actual discharge, if calibration estimates of actual high, medium, and low discharges
111 can be obtained while sustained width-sensitive observation is underway (Smith,
112 1997; Brakenridge et al., 2007).

113 As is the case for gauging stations on the ground, the local river and floodplain
114 channel geometry control the accuracy of rating curve relations in a satellite-based
115 approach. For stage-based measurements at gauging stations, a desirable site
116 exhibits stable channel geometry with relatively permanent and steep channel
117 banks, where discharge changes are accommodated mainly by changes in d and
118 stage. For observation via satellite, w changes can be most frequently observed, and
119 a desirable measurement site is one where discharge changes are accommodated
120 mainly by changes in w . Most river systems exhibit reaches of both types. Some
121 rivers are in fact difficult to monitor by gauging stations due to variable channel
122 geometry, meandering or braiding channels, and other dynamic processes. Remote

123 sensing responsive to w , (or, for a defined reach, flow area) offers a potentially
124 better approach at such locations.

125 In this regard, there are actually two alternatives for sensing changes in river
126 “width”: 1) measurement of actual flow width changes, at individual cross sections
127 (Bjerklie et al., 2003), or 2) remote sensing signal measurements that are sensitive
128 to flow area change, along a defined measurement reach (Smith, 1997). Monitoring
129 water surface area is particularly attractive, because it takes advantage of the spatial
130 coverage provided by remote sensing. Reach surface water area is also less prone to
131 local variation in riverbed geometry, due to accomodating the net effects of local
132 scour and fill. In contrast, measuring flow width is observationally demanding,
133 because of the dual challenge of high spatial resolution and frequent sampling in
134 time. Furthermore, high-resolution characterizations of a river at specific cross
135 sections would require frequent recalibration due to seasonal, annual, and inter-
136 annual changes in riverbed, location, and meandering patterns (just as stage rating
137 curves do). This paper employs the second approach, which is most appropriate for
138 remote sensing from above: using sensors that are sensitive to flow area change,
139 have frequent revisit characteristics, and with sufficiently high spatial resolution to
140 record small flow area changes.

141 River discharge can also be modeled instead of observed: by
142 parameterization of catchment areas and measurement of forcing variables,
143 including precipitation. This independent approach offers an opportunity to
144 calibrate the remote sensing to discharge values. Through modeling, if changing
145 catchment precipitation, soil moisture, evapotranspiration, and other upstream

146 watershed characteristics can be measured or constrained, reasonably accurate
147 discharge can be estimated and for potentially unlimited locations along a river. As
148 daily precipitation and other data fields are ingested, updated model-based
149 discharge estimates can be calculated at the same time intervals. Contemporary
150 watershed runoff modeling uses advanced computational capabilities to scale flow
151 routing and other functions to relatively fine scale watershed characterizations (e.g.
152 to a global grid at approximately 10 km).

153 This paper considers whether global hydrology model-based discharge
154 information can provide the needed calibration of remote sensing observations.
155 Such capability would enable sustained satellite characterization of river discharge
156 via either flow area or (from altimetry) stage, and where *in situ* data are unavailable.
157 We analyze a suite of 6 river measurement sites within the U.S. where surface
158 gauging station, remote sensing, and model results are co-located. First, the
159 temporal sampling needed to adequately characterize river flow variation is
160 considered. Next we describe the passive microwave remote sensing that provides
161 the needed measurements. In order to test ground-based versus model-based
162 calibration outcomes, we employ the WBM water balance model (Wisser et al.,
163 2010; Wisser et al., 2008) and obtain predicted daily discharges for the
164 measurement sites. Rating equations for the remote sensing signal are developed
165 and compared via two different methods: 1) using modeled discharge values, and 2)
166 using ground station-measured discharge. The co-location with gauging stations
167 also allows constraints to be placed on the accuracy of satellite-based discharge
168 measurements using either approach.

169 3. Temporal Sampling for Discharge Characterization

170 Earth-observing satellites are currently being planned to help measure global
171 river discharge and water storage changes and constrain runoff modeling (Alsdorf
172 et al., 2003; Alsdorf et al., 2007; Durand et al., 2008; Durand et al., 2010). Potential
173 remote sensing revisit frequencies for any given river location vary widely: from
174 hourly, for geostationary satellites, to ~ weekly, for low latitude locations in the
175 proposed Surface Water and Oceans Topography (SWOT) mission (Biancamaria et
176 al., 2010). Because of the constellation of sensors planned or already available, there
177 are clear opportunities for complementary measurements, in which more-precise
178 but relatively infrequent observational data from experimental missions are
179 combined, when available, with less precise but ongoing and frequent surveillance
180 of rivers by operational systems.

181 The minimum temporal sampling needed to adequately characterize river flow
182 varies with river flow regime. Along some very large rivers, where the daily
183 discharge is strongly auto-correlated and the rate of change is not fast, sampling
184 frequency requirements may not be high. As a result, except during major flooding,
185 surface stations that provide a daily record may actually oversample. However,
186 water discharge for most rivers is a rapidly varying flux, at least during part of a
187 season (Shiklomanov et al., 2006). Thus: 1) a 10-fold discharge change may occur
188 along many rivers over a period of only several days, or less, and 2) a large
189 proportion of total annual river runoff may be concentrated in flood seasons lasting
190 only several weeks to several months. Also, measuring low flow during a sustained
191 drought, or high flow during a flood, requires sustained high frequency observation:

192 the duration of extreme flow in days is as important as high precision individual
193 measurements in obtaining total monthly runoff. Shiklomanov et al (2006),
194 analyzing Arctic rivers, describe in detail this strong dependence on sampling
195 frequency in measuring accurate values for even total annual runoff.

196 Although stage-discharge rating curves exhibit various errors, including
197 hysteresis (Dottori et al., 2009), transformation of frequently or continuously
198 measured stage to estimate discharge has long been accomplished within acceptable
199 and well-constrained accuracy and precision. An inherent motivation of this overall
200 approach is close-interval sampling in time. In some cases (e.g. flood hydrographs
201 along smaller rivers), the time scale may be hours, but the large proportion of
202 ground station-based river discharge data is reported using daily time intervals. An
203 important challenge for remote sensing of river discharge is to achieve at least this
204 same frequent sampling in time while progressively improving, with better sensors
205 and processing techniques, the accuracy of individual (daily) measurements.

206 **4. Passive Microwave Radiometry for River Discharge Measurement**

207 One reason for utilizing microwave information is that, at selected
208 frequencies, microwave radiation suffers relatively little interference from cloud
209 cover. Also, night overpasses can be utilized; the signal does not require solar
210 illumination. These attributes allow for frequent data retrievals on a global basis
211 (e.g. pixel spatial resolutions of ~10km, daily or near-daily repeats).

212 Factors that affect total upwelling microwave brightness from a mixed water
213 and land surface measured by a single image pixel include: a) sensor calibration

214 characteristics (stability of its signal through time), b) perturbation of the signal by
215 land surface changes (e.g., surface temperature, soil moisture, crop changes,
216 snowfall, and rainfall), and c) contrast between land and water at the frequency
217 being used (very different values of emissivity for water and land favor the most
218 sensitive monitoring of water area change). Also, microwave frequencies have more
219 commonly been used to observe soil moisture changes (Schmugge, 1980; Theis et
220 al., 1982; Ulaby et al., 1978; Wang et al., 1982; Wang et al., 1980; Njoku et al., 2003;
221 Nghiem et al., 2012). Because of the sensitivity of microwave emission to soil
222 moisture as well as surface water, measurements of surface water change must
223 incorporate some method to remove variations caused by temporal changes in soil
224 moisture.

225 The fundamental basis of passive microwave sensitivity to river discharge for
226 mixed water/land pixels was analyzed with a microwave emission model derived
227 from first principles (Brakenridge et al., 2007). The emission model is developed
228 from fluctuation-dissipation theory, incorporating the non-isothermal conditions of
229 riverine environments. Correlations of electromagnetic fields derived from
230 Maxwell's equations with different signal polarizations can be cast in form of a
231 hyperbolic cotangent factor of the quantum energy ($\hbar\omega$) over the absolute physical
232 temperature (Tsang et al., 1985), operated on a tensor product involving the
233 polarization vector, complex effective permittivity, and dyadic Green's function
234 (Nghiem et al., 1990).

235 A difficulty in interpreting the microwave radiance measured by a satellite is
236 that it is a product of both physical temperature and emissivity. Whereas the

237 emissivity contains water information, the physical temperature can change quickly,
238 depending on time of the day, solar shading (e.g., topographic shadowing), and
239 weather conditions. Whereas many passive microwave methods use the
240 polarization ratio (PR) and the frequency gradient ratio (GR) to cancel physical
241 temperature within a pixel, PR and GR also reduce the sensitivity to water change
242 (Brakenridge et al., 2007). The key for river discharge measurement is to cancel the
243 physical temperature, also using a ratio approach, but with the river measurement
244 pixel amplitude value compared to nearby but separate calibration pixel values. This
245 approach retains a high sensitivity to river discharge variability expressed as water
246 surface area changes (Brakenridge et al., 2007).

247 Finally, the reach water surface area rather than flow width approach also
248 greatly relaxes the spatial resolution requirements for sensing flow variation. The
249 microwave signal from a defined river reach, and geographically including both: a)
250 lower channel water area, and b) upper channel bar surfaces and floodplain dry
251 land, will track discharge: as the river rises and falls, the reach water and land
252 proportion changes, and only a sensitive numeric indicator of such is needed. An
253 actual map of water versus land is not required. The microwave signal variation
254 from individual, relatively large (~ 10 km) pixels centered over rivers can thus be
255 used directly: the measured reach is one such pixel (Brakenridge et al., 2007). This
256 approach in fact requires relatively large image pixels, because it is important that
257 the highest floods not completely fill or saturate a pixel. The sensitivity, noise
258 characteristics, and stability of the remote sensing signal are, however, critical, and
259 the remote sensing data must be accompanied by high quality geocoding: any

260 variation in the actual ground surface being sampled by repeat measurements
261 introduces noise.

262 **5. Geographic Sampling Considerations for Global Measurements**

263 For global characterization of freshwater runoff through rivers, a large array
264 of sites, at least several thousand, is needed: this still provides only several hundred
265 per continent and leaves many major streams and rivers un-monitored. There are
266 many potential issues involved with efficient design of gauging station networks
267 sampling global scale land areas. For example, although a set of relatively few
268 gauges located near the mouths of large rivers can capture a considerable portion of
269 the total discharge to oceans (Fekete et al., 2002), the remaining contributing
270 landmasses are fragmented into hundreds of small watersheds. Also, discharge
271 should best be measured just downstream of the confluences of tributaries, because
272 discharge varies downstream only gradually along trunk streams, whereas
273 tributaries typically add a large sudden increment that is important to capture.

274 Design criteria for global sampling schemes are beyond the scope of this
275 paper. However, previous MODIS imaging of global surface water variability
276 (Brakenridge et al., 2005; Brakenridge and Kettner, 2012) provides abundant (n=
277 2583) suitable locations where flow area variation has already been measured
278 optically on an intermittent basis (Figure 1). At these locations, it has been
279 demonstrated that a water area-sensitive remote sensing signal will monitor flow
280 variability. These potential measurement sites are thus a useful starting point in
281 designing a global array.

282 Microwave signal data for these and additional sites (De Groeve, 2010; De
283 Groeve et al., 2006; De Groeve and Riva, 2009; Kugler and De Groeve, 2007) added
284 more recently are available at: <http://www.gdacs.org/flooddetection/>. The
285 sensitivity of each measurement site to discharge variation, and the character of
286 each site's signal-to-discharge rating curve, are both a function of individual site
287 characteristics, and especially channel and floodplain morphology. An efficient
288 calibration approach is needed to convert these numerous discharge-sensitive
289 records to discharge units.

290 **6. Choice of Data and Processing Strategies**

291 The data available to monitor rivers in the microwave domain includes the
292 37 GHz channel provided by the SMMR (Scanning Multichannel Microwave
293 Radiometer) in 1978-1987, the SSM/I (Special Sensor Microwave Imager) aboard
294 the Defense Meteorological Satellite Program satellite series (1987 to present), the
295 37 GHz channel aboard TRMM (Tropical Rainfall Measurement Mission, 1998 to
296 present), similar frequency but including V/H polarimetric data provided by AMSR-
297 E, (Advanced Microwave Scanning Radiometer for Earth Observation System) July,
298 1, 2002-October 4, 2011, and the recently launched (early 2012) AMSR instrument
299 aboard the Japanese satellite GCOM-w. Most data from these sensors are made
300 available in swath image formats (not geolocated into map projections, but with
301 accompanying latitude and longitude coordinate information for each pixel) and
302 also as geocorrected raster images (pixels of fixed dimensions and geographic
303 location within global or large-region raster files).

304 In this study, we describe two passive microwave *data sources* and also two
305 *signal processing methods*. However, the comparisons use mainly one data source
306 and one method: AMSR-E data processed according to the first method, below. It
307 was used prior to transition to the second method in the current processing scheme.

308 *Method 1* uses AMSR-E 36.5 GHz, horizontal H polarization, descending orbit
309 (night) data, as obtained by a swath image pixel value retrieval algorithm (De
310 Groeve et al., 2006). In this algorithm, data from within a 5 km radius of a
311 geographic point target are retrieved, as determined by the geolocation information
312 for each pixel (the values obtained are from pixels whose centers are within that
313 radius). The river measurement reaches (the “M” data) are, therefore, circular in
314 shape. Also, information from a fixed and nearby (dry land) comparison site (the “C”
315 data) is retrieved from the same swath image and includes an area of identical size,
316 manually selected to be free from mapped streams and rivers. M/C, a dimensionless
317 ratio value, is the discharge estimator; as noted, use of the ratio isolates any change
318 that affects only one of the pixels and, in particular, river flow area variation. Data
319 processed in this way show a strong correlation to measured discharge at many
320 sites in the U.S. (Figure 2A, Figure 3).

321 *Method 2* uses AMSR-E 36.5 GHz, total amplitude (V and H polarizations
322 combined), and including data from both ascending and descending orbits, as
323 mosaicked within georeferenced, global-coverage, near real time raster images.
324 These image data are in latitude and longitude (Plate Carree) projection, with pixel
325 dimensions of .0833 degrees (approximately 9.27 km square at the equator but
326 with decreasing east-west km dimensions at increasing distances from the equator).

327 The processing, as automatically performed by the Global Flood Detection System in
328 Ispra, Italy (De Groeve, 2010; De Groeve and Riva, 2009), also calculates a
329 dimensionless ratio value from these rasters, but the comparison value is based on
330 the brightest (driest) values from a 7 x 7 pixel array in the raster and centered on
331 the measurement pixel. The measurement pixels each contain the same latitude and
332 longitude point targets as for the first method, but the fixed pixel ground footprint
333 means that the river reach being sampled differs significantly (with a maximum shift
334 of a half pixel size, or about 5 km). This approach does not require the manual
335 selection of the calibration pixel, making it computable anywhere in the world. Its
336 other advantage is that single-pixel variation in the calibration information cannot
337 so strongly affect the discharge-estimator signal. In detail, the algorithm calculates
338 the (95th percentile) brightest value of the calibration pixels and the ratio of that
339 value to the measurement pixel value (Figure 2B, Figure 3). Previous comparisons of
340 the two methods for other sites indicate the results to be strongly correlated (Figure
341 2) and to exhibit comparable amounts of scatter and error (De Groeve and Riva,
342 2009).

343 In both processing methods, a 4-day forward running mean is applied,
344 because AMSR-E does not provide daily revisits at lower latitudes. Instead, some
345 locations commonly are revisited every two days, or, very rarely, only every three
346 days, as the AMSR-E orbit precesses. The 4-day running mean facilitates a most-
347 current update, daily, with values for every location globally. In any comparisons to
348 ground station data or model output, therefore, we also use 4 day running mean
349 data. Future microwave sensors such as NASA's planned GPM mission will provide

350 more-than-daily revisits and thus a daily update without multi-day averaging will be
351 possible at all latitudes.

352 The AMSR-E data offer the capability to consistently monitor river
353 measurement sites for nearly a decade (data begin in July, 2002) and for ground
354 footprints of approximately 10 km; however, the sensor ceased operation on
355 October 4, 2011. The 37 GHz frequency and H polarization were selected in method
356 1 because H polarization data exhibits the strongest differential response to water
357 and land (Brakenridge et al., 2007) at this frequency and with lesser sensitivity to
358 soil moisture. The ongoing TRMM satellite output provides similar microwave data
359 (but from a non-polar orbit, and without high latitude coverage). The signal
360 processing at GDACS/GFDS is presently using these TRMM data; as noted, the
361 methods described are also applicable to an array of similar frequency remote
362 sensing from other sensors.

363 **7. The WBM global hydrology model**

364 The WBM model includes the water balance/transport model first
365 introduced by (Vörösmarty et al., 1998; Vörösmarty et al., 1989) and subsequently
366 modified (Wisser et al., 2010; Wisser et al., 2008). WBM is a relatively simple but
367 robust water budgeting scheme that takes into account climate forcings (air
368 temperature and precipitation in its simplest form) and estimates various water
369 stocks (soil moisture and groundwater) and fluxes (evapotranspiration, surface
370 runoff, groundwater recharge and baseflow). WBM has been applied successfully in
371 small watersheds at 200m spatial resolution, up to a global scale at 6 minute grid

372 (approximately 11 km at the equator) cell sizes. WBM was probably the first
 373 hydrological model applied to a global domain. The main difference between WBM
 374 and comparable large-scale hydrological models is the high degree of flexibility in
 375 specifying computation domains and input data and configuration. WBM has
 376 demonstrated a bias of 5-8mm/yr (Fekete et al., 2002; Vörösmarty et al., 1998) with
 377 respect to annual runoff (297mm/yr). Numerous studies have shown that the most
 378 critical input variable is precipitation (Fekete et al., 2004; Biemans et al. 2009).

379 At its core, the surface water balance of non-irrigated areas is a simple soil
 380 moisture budget expressed as:

$$381 \quad dW_s / dt = \begin{cases} -g(W_s)(E_p - P_a) & P_a \leq E_p \\ P_a - E_p & E_p < P_a \leq D_{ws} \\ D_{ws} - E_p & D_{ws} < P_a \end{cases} \quad (2)$$

382 driven by $g(W_s)$, a unitless soil function:

$$383 \quad g(W_s) = \frac{1 - e^{\left(-\alpha \frac{W_s}{W_c}\right)}}{1 - e^{-\alpha}} \quad (3)$$

384 W_s is the soil moisture, E_p is the potential evapotranspiration, P_a is the precipitation
 385 (rainfall P_r combined with snowmelt M_s), and D_{ws} is the soil moisture deficit: the
 386 difference between available water capacity W_c , which is a soil and vegetation
 387 dependent variable (specified externally) and the soil moisture. The unit-less
 388 empirical constant α is set to 5.0 following Vörösmarty et al. (1989).

389 Flow routing from grid to grid cell follows the downstream grid cell tree
 390 topology (which only allows conjunctions of grid cells upstream, without splitting to

391 form islands or river deltas) and is implemented using the Muskingum-Cunge
392 equation, which is a semi implicit finite difference scheme to the diffusive wave
393 solution to the St. Venant equations (ignoring the two acceleration terms in the
394 momentum equation). The equation is expressed as a linear combination of the
395 input flow from current and previous time step ($Q_{in\ t-1}$, $Q_{in\ t}$) and the released water
396 from the river segment in the previous time step ($Q_{out\ t-1}$) to calculate new grid-cell
397 outflow:

$$398 \quad Q_{out\ t} = c_1 Q_{in\ t} + c_2 Q_{in\ t-1} + c_3 Q_{out\ t-1} \quad (4)$$

399 As described by Wisser et al., 2010), the Muskingum coefficients (c_1 c_2 c_3) are
400 estimated from channel properties (width, depth, slope, and length) using the
401 relations of Cunge (1969) and Dooge et al. (1982). We use a power function
402 approximation of channel geometry $w = a y^b$ to express the relationship between the
403 width (w) and depth; b dictates the ratio and of flood-wave celerity to flow velocity.

404 In this paper, the WBM water discharge predictions are from a daily, global
405 scale simulation at 6 arc-minute (~ 11 km) spatial resolution. Daily predictions are
406 averaged by a 4 day running mean window to align with the satellite microwave 4
407 day averaging process. The precipitation dataset is from the Global Precipitation
408 Climate Center GPCC, Offenbach, Germany (gpcc.dwd.de) using their “Full” product,
409 which combines long-term precipitation climatology, derived from the entire data
410 archive, with anomalies estimated from the operating meteorological stations at any
411 given time. The GPCC “Full” product is available at monthly time steps at 30 arc-
412 minute spatial resolution. Daily partitioning of the monthly precipitation totals was

413 established by computing the daily fraction of the monthly precipitation from the
414 NCEP reanalysis product (Kalnay et al., 1996; Kistler et al., 2001). A six minute
415 topological network (Vörösmarty, Fekete, Meybeck, & Lammers, 2000) was derived
416 from the high resolution gridded network HydroSHEDS using SRTM elevation data
417 set (Lehner, Verdin, & Jarvis, 2008). A comprehensive list of the model input
418 datasets is provided (Cohen et al., 2011).

419 **8. Testing WBM Model Output For Rating Curve Generation**

420 The United States is monitored by a relatively dense array of operational
421 hydrological gaging stations. Data from these allow us to evaluate the effectiveness
422 of a model-based approach to calibrate remote sensing measurements to discharge
423 values.

424 We chose 6 sites for satellite-based measurement in the continental U.S.
425 (Figure 4) that are coincident to or in very close proximity with *in situ* stations
426 providing daily measurements between 2002-2010. The site locations and
427 attributes represent diverse geomorphological, land-use and climate settings (Table
428 1). Although this is a small number of sites, their analysis provides the opportunity
429 to consider in detail the relationship of the remote sensing to station-observed
430 discharge variation and that provided by the model.

431 For each site, the empirical relation (the rating curve) between the remote
432 sensing signal and ground station-measured water discharge is constructed. As well,
433 the signal is compared to coeval model results, to produce a separate and
434 independent model-based rating curve for each site. This would be one method for

435 calibrating thousands of river measurement sites distributed globally (Figure 1). By
436 comparing the rating curves, and the resulting discharge time series, we can
437 investigate how accurately satellite sensors can measure discharge, *if the signal is*
438 *calibrated only from global modeling results:* without any ground-based information.

439 Three temporally coincident datasets are used in each case (Figure 5):

- 440 1. Daily, including the complete (9 year) daily values (n = 3285);
- 441 2. Monthly, including the monthly mean, maximum and minimum daily values
442 for 12 months (n = 36);
- 443 3. Yearly, including the annual mean, maximum and minimum daily values (n
444 =27).

445 For consistency, second-order polynomial rating curves are used to evaluate the
446 scatter plots created in all cases (Table 2). We compared our results using other
447 regression equations without substantial change in the results. Because of relatively
448 large scatter at the lower end of some river discharge regimes (the flow area
449 method becomes less sensitive once flow is fully confined within the lower channel),
450 there is an additional requirement that all portions of the polynomial curve remain
451 monotonic or flat.

452 We seek also to determine the optimal calibration strategy (daily, monthly or
453 yearly values) that could be applied to a large number of sites. Figure 6 shows daily
454 water discharge time-series (2002-2010) for the six sites and as based on both
455 model-based and station-measured calibrations. The plots also include the
456 measured discharge at the co-located gaging station (Figure 4 and Table 1) for

457 comparison. The top plot for each site is obtained from the daily data rating curve;
458 the middle from calibration with monthly statistics; and the bottom from yearly
459 statistics (e.g., figures 5a, 5b and 5c respectively). Black lines in Figure 6 show the
460 ground station-measured discharge; blue lines the satellite results based on using
461 ground station data for the rating curves, and red lines the satellite results which
462 use model output for the rating curves.

463 Overall, visual comparison of the remote sensing signal to station-measured
464 discharge yields a generally strong time series correlation. Figure 4 also provides
465 such comparison on an expanded temporal scale; the applicable Nash-Sutcliffe
466 values are .60 and .61. In the Figure 6 plots, however, we are concerned with
467 understanding how the choice of calibration, via rating curves, affects the discharge
468 results. Calculating the Nash-Sutcliffe descriptive statistic assists in this regard:
469 higher values should indicate more correlated results (without further
470 consideration of other factors bearing on such statistics, including autocorrelation,
471 time lags, data distributions, influence of outliers, etc).

472 From Figure 6, discharge estimation based on daily data calibration (rating
473 curves such as in Figure 5a) is similar to that obtained when the rating curve uses
474 monthly and yearly statistics: if station data rather than modeling are used for the
475 rating curve. Nash-Sutcliffe values range among the sites between .11-.37 (satellite-
476 observed, compared to gauging station data). In contrast, discharge values obtained
477 from model-based calibration methods (dashed orange lines in Figure 6) can vary
478 depending on whether daily versus yearly or monthly data are used for the rating

479 curves, and also there is more variability by site: the modeling, as expected, is more
480 accurate at some sites than at others.

481 In this regard, modeled daily data-based rating equations predict lower than
482 observed discharge (most clearly in site #530; Figure 6). Comparison of WBM model
483 results to measured discharge further indicates that the model itself generally
484 under-predicts mean discharge (Table 1). In sites #997 and #2483, the daily data-
485 based rating curve produces more accurate results than monthly and yearly
486 calibrations (e.g., for #997, Nash-Sutcliffe values of .2 for the daily-based calibration
487 compare to -1.0 for the monthly and yearly). In these two cases, WBM considerably
488 over-predicted high discharge events (Figure 6).

489 The results overall demonstrate the sensitivity of any model-based
490 calibration approach to the accuracy of the model predictions. They indicate that
491 using yearly and monthly statistics to calibrate the AMSR-E signal data to discharge,
492 in most cases, better constrains the size of very high discharge events: even though,
493 for some events, there is over-estimation of the flood magnitude (i.e. sites 997 and
494 2483; Figure 6). WBM Model-based calibration, in general, is found to be a viable
495 approach for translating the remote sensing signal to discharge, and we find no
496 major advantage in using daily information rather than monthly or yearly mean,
497 maximum, and minimum values, as defined above, and within this analyzed 9 year
498 period of record.

499 To further evaluate errors associated with the method 2 data and associated
500 processing, daily station-measured and remote sensing-measured values ($n = 1824$)

501 were obtained for one site (#524), 2003-2006 using the model-based, monthly
502 value-based rating curve. Assuming the gauging station data as representing true
503 discharge, the average error departure of the remote sensing (daily-incremented)
504 discharge values is 67%, with percentage errors being largest at times of low flow.
505 These relatively large daily value errors are reduced in the calculation of runoff
506 totals from these data, and in part because high error values at low flows less
507 strongly affect runoff totals. For annual values 2003-2008, the average error is 9%.

508 Previous work (Brakenridge et al., 2007) indicates one source of error in the
509 daily values produced by this remote sensing technique is the lack of exact temporal
510 match between station and remote sensing discharge series. For example, major
511 flood peak discharge as measured by surface gauging stations may precede by 1-2
512 days the peak recorded by remote sensing (which is measuring reach flow area
513 along an entire river measurement site). Such lags produce a negative departure
514 (remote sensing value – station value) as the peak flow passes the station and while
515 the reach area is progressively flooding. Then, several days later, a positive error
516 occurs as stage is already declining at the station (in part due to the overbank flow).
517 Thus, the peak discharge value may be recorded accurately by both ground-based
518 stage and satellite-based flow area techniques, but the timing may differ and lead to
519 large increases in the average daily measurement error and in descriptive statistics
520 such as the Nash-Sutcliffe coefficient.

521 **9. Modeling and Remote Measurement of an Extreme Flood**

522 As noted, for many locations globally, daily discharge information from
523 surface gauging stations is difficult or impossible to obtain. Even where gauging
524 station data are available and are public, large floods can temporarily damage or
525 entirely disable surface stations. Although orbital remote sensing can, presently,
526 provide valuable river discharge information and monthly and annual runoff
527 volumes, there are significant errors still to be addressed (examine the time series
528 shown in figures 3 and 6). Perhaps the greatest asset of the remote sensing
529 capability here detailed is its ability to be quickly and easily applied to new
530 measurement sites of interest, without field access. An example is now presented to
531 enable further examination of the utility of satellite microwave river discharge
532 measurements in general, and those based on WBM model calibration in particular.
533 The results further emphasize that accurate remote sensing measurement via this
534 approach will depend on the quality of any hydrological model used for calibration.

535 During the summer monsoon of 2010, The upstream Khyber-Pakhtunkhwa
536 region of Pakistan experienced rainfall totals >300 mm July 27-30, and the Punjab,
537 Gilgit Baltistan and Azad Kashmir provinces received July rainfall totals of >500
538 mm. The trunk stream (Indus) flood hydrograph then traversed 500 km of river
539 reach to the sea, mainly along a meandering channel that is constrained within a 15
540 to 20 km wide floodplain by engineered artificial levees. All of this floodplain (and
541 more) was inundated (Syvitski and Brakenridge, submitted manuscript).

542 Analysis of optical remote sensing data indicates that most damage was
543 caused by multiple failures of irrigation system levees, and by barrage-related
544 backwater effects that initiated failures and led to avulsions (sudden changes in flow

545 location). We consider here the difference between the modeled and the remotely-
546 observed flood hydrograph at an illustrative remote sensing measurement site.

547 The WBM-modeled peak discharge for this flood at site #2010, south of a
548 major levee failure and partial avulsion of the Indus at the Tori Bund, is $\sim 26,000$
549 m^3/sec , with flow being elevated above $15,000 \text{ m}^3/\text{sec}$ for only several days (Figure
550 7). However, the model includes no limitations on the volume of water transported
551 in a river at a point in time (no change to overbank flow conditions is incorporated).
552 This can cause over-prediction of the magnitude of high flow events (as shown in
553 the U.S. sites #997 and #2483; see also Cohen et al., 2011). Also, the modeled water
554 is transported much too rapidly downstream. A new version of WBM (currently in
555 testing) will address these limitations by incorporating an over-bank flow
556 component that acknowledges the reality of channel overtopping during large
557 discharges. Also, the present model does not include the possibility of avulsion.

558 Comparison of the remotely sensed discharge at station #2009, upstream of
559 the avulsion at Tori, and at #2010 indicate a reduction of measured peak flow
560 downstream of the breach by $\sim 10,000 \text{ m}^3/\text{sec}$ (Syvitski and Brakenridge, submitted
561 manuscript). Figure 7 shows the very different shape of the observed hydrograph at
562 this site compared to that modeled for it. Thus, avulsion reduced the peak flow, and,
563 also, the flood was experienced for much longer (22 days of $> 15,000 \text{ m}^3/\text{sec}$) than
564 the model predicted. During large floods, and even along heavily engineered rivers,
565 major attenuation of the flood wave typically occurs, and this is illustrated in the
566 Indus example. This attenuation can be measured in detail by this form of remote
567 sensing. However, its adequate characterization by modeling at this spatial scale

568 remains an important task for future work. The lack of accurate modeled peak
569 discharge for extreme events may in turn generally affect model-based rating curves
570 and the remote sensing-assessment of peak discharge magnitudes.

571 **10. Conclusion**

572 The results indicate that microwave satellite discharge characterization at
573 selected river reaches can approach *in-situ* ground station information in its utility
574 for several applications, including the analysis of flood dynamics and the
575 quantification of longer term watershed runoff volumes. However, remote sensing
576 of rivers through these methods does require some form of calibration to discharge
577 values via rating equations. The examples we analyzed indicate that the needed
578 transformation of water-area sensitive remote sensing to river discharge can be
579 accomplished by incorporation of global runoff model results. Using the described
580 or similar microwave data and processing approaches, and for river measurement
581 sites whose channel and floodplain morphologies favor flow area variability, 4-day
582 running mean daily discharges as measured via satellite compare favorably with
583 information obtained by gauging stations. The timing and duration of periods of
584 high and low flow are accurately constrained, and the relative magnitude in m^3/sec
585 of flood peaks can be determined. However, daily value accuracies exhibit
586 significant errors, in part due to a lack of exact temporal match in the timing of some
587 major flood peaks. For annual runoff expressed in mm/yr , observed errors, at the
588 suite of sites examined, and using a global model-based calibration approach was
589 relatively small. This suggests that the measurement technology is already able to

590 deliver significant new information for water balance studies at many international
591 locations, and without support by ground-based information.

592 We stress the synergy between different remote sensing approaches for
593 discharge measurement. One upcoming space agency mission (the U.S./France
594 SWOT satellite) is being designed to provide global data sets of accurate swath radar
595 altimetry-based river stage and slope, but without a long-term record and with a
596 short (3-year) nominal mission life. Flow area measurements through existing and
597 planned microwave sensors can, meanwhile, be made frequently (\sim daily); they can
598 potentially be extended back about three decades in time at favorable sites, and they
599 can be continued while SWOT is collecting data and afterwards. Several satellites
600 are currently providing appropriate, stable, well-calibrated, water area-sensitive
601 data; these can already be used. For many research efforts and well as practical
602 applications, both long-term data and current near-real-time observations are
603 necessary. The challenge is to develop processing methodologies that can ingest,
604 process, and disseminate the results, provide reliable error estimates, and allow
605 synergistic incorporation of new sensor data when such become available.

606 In regard to the best calibration/rating curve approaches, our analysis
607 indicates significant variation in the rating curve equations, depending on whether
608 model-based daily, monthly or yearly statistics are used. In general, daily data-based
609 rating curves do not always accurately estimate the highest flow events: polynomial
610 or other regressions applied to the comparisons of modeled and observed daily data
611 from the calibration period may not accurately capture the relation between the
612 largest discharge and the remote sensing signal, and especially when the modeled

613 routing of flood waves inadequately captures overbank and other flow attenuation
614 processes. Rating curves based instead on monthly or yearly maximum and
615 minimum statistics better characterize the signal/discharge relation at the
616 extremes. Preliminary work using the method 2 data and processing indicates that
617 incorporating a 5 year period of record for both modeled and observed values, and
618 using monthly daily maxima, minima, and mean values ($n = 180$) commonly
619 produces rating curves with monotonic, second order polynomial least square
620 regression r^2 values $>.6$ at favorable sites, and also provides the most accurate
621 prediction of peak flow values.

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628 for computing time on high-performance computing clusters.

629

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757
758

759 **Figure Captions**

760

761 Figure 1. Satellite river measurement sites (n = 2583) where optical remote sensing
762 (2001-2010) detects significant surface water area variation within the site reaches (10
763 km in length). Near-daily time series of passive microwave signal have been obtained and
764 archived for each site since July 1, 2002. Evaluation of the 10 yr+ time series allows the
765 daily signal data to be binned into low flow (yellow dots, <5th percentile of complete
766 series), normal flow (blue dots), moderate flood (purple dots, recurrence interval > 1.33
767 yr via Log Pearson III) and large flood (bright red dots, > 5 yr recurrence via Log Pearson
768 III). Red dots at high latitudes are processing errors due to ice-covered conditions.

769

770 Figure 2. A (top), Plot of the microwave discharge estimator ratio, 4-day running
771 means, calculated according to method 1, for each day, January 1, 2009-December
772 31, 2010, versus 4-day forward running mean gauging station discharge, White
773 River, southern Indiana (remote sensing site 524; gauging station USGS 03360500
774 White River at Newberry, Indiana). B (bottom), Plot of the estimator ratio,
775 calculated according to method 2, versus the gauging station information, same time
776 period. Vertical scales are in ft^3/sec .

777

778 Figure 3. A, top: satellite-estimated daily 4-day running mean river discharge, site 524,
779 in red, compared to 4-day running mean discharge measured at the co-located gauging
780 station (blue). Rating curve was based on comparison of daily station and (method 2)
781 satellite data; applicable Nash-Sutcliffe statistic is .60. B, bottom: satellite-estimated
782 discharge, red, using a rating based on the WBM model-produced discharge information
783 (same remote sensing data); applicable Nash-Sutcliffe statistic is .61. The model-based
784 rating curve underestimates peak discharge but characterizes average flow conditions
785 quite accurately. Vertical scales are in ft^3/sec .

786

787 Figure 4. Location map for the remote sensing river measurement sites and co-located
788 USGS gaging stations.

789

790 Figure 5. Example plots (site #925) of method 1 microwave discharge estimator
791 values versus WBM-simulated discharge. A, top: Daily values using the entire dataset.
792 B, middle: Monthly values (monthly mean, minima and maxima). C, bottom: Yearly
793 values, using only yearly mean, minimum and maximum. The daily value-based rating
794 equation underestimates flood flows.

795

796 Figure 6. Nine year (2002-2010) daily time series of water discharge for the 6 remote-
797 sensing sites (numbering corresponds to Figure 4 and Table 1). Gauging station-measured
798 discharge is plotted with a thick black line, microwave signal-estimated discharge based
799 on the gauging station data is plotted with a blue line, and microwave signal-estimated
800 discharge based on WBM model-predicted discharge is plotted with a dashed orange line.

801 The top plot for each site is for calibration using the entire daily dataset, the middle plot
802 is for calibration using only the monthly statistics and the bottom plot for calibration
803 using only yearly statistics.

804

805 Figure 7. Time series for the year 2010 showing the time lag between WBM-simulated
806 and microwave-observed discharge (dashed black and solid blue lines respectively) at site
807 #2010 on the Indus River, Hala, Pakistan. Modeling predicts an earlier and higher flood
808 crest, and more rapid dissipation than was observed via remote sensing.

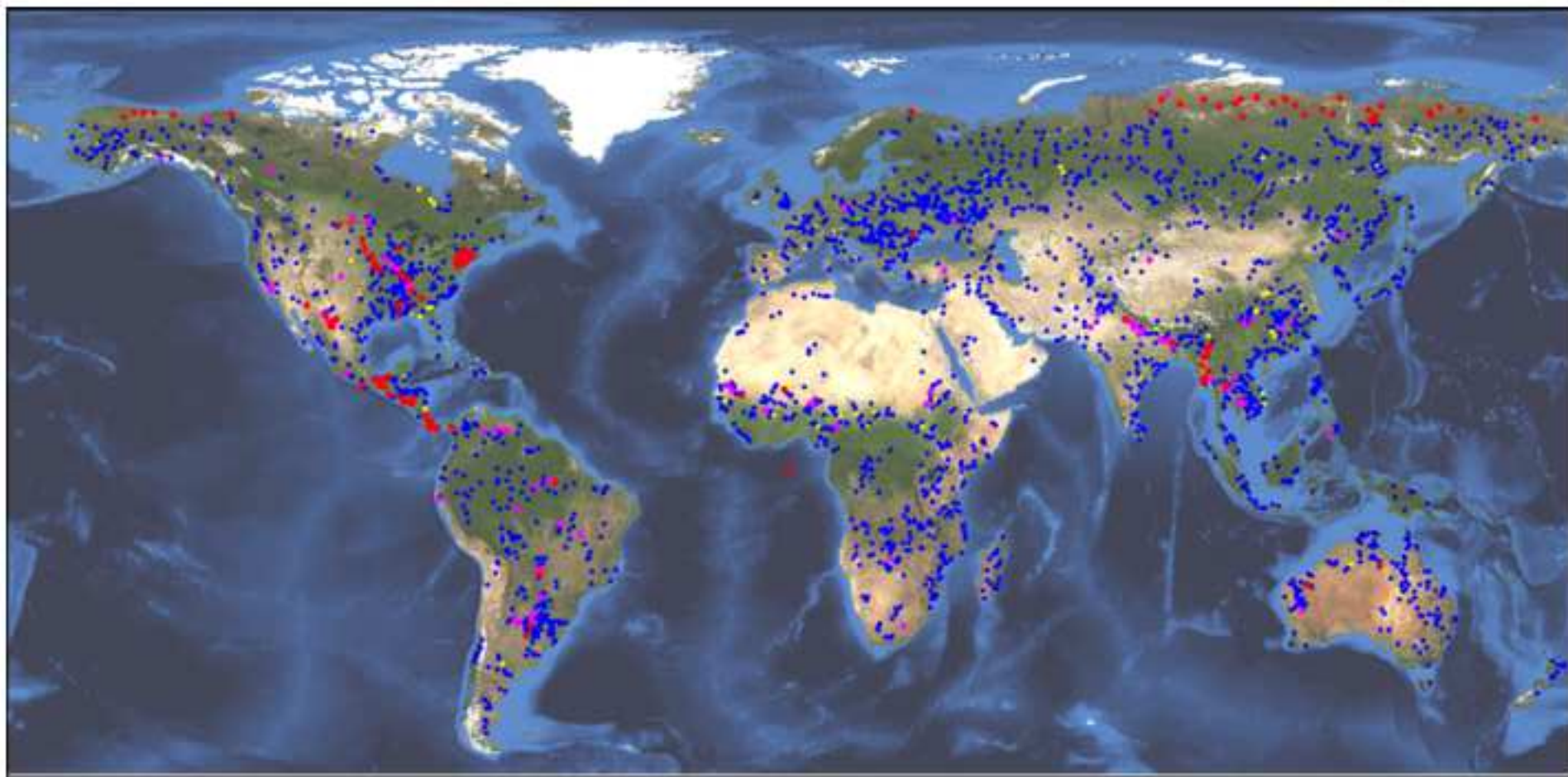
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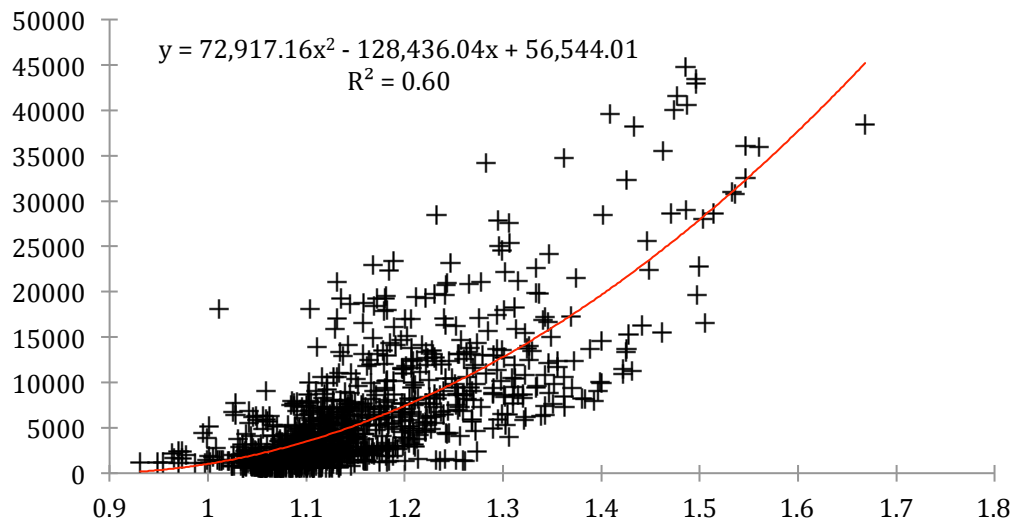
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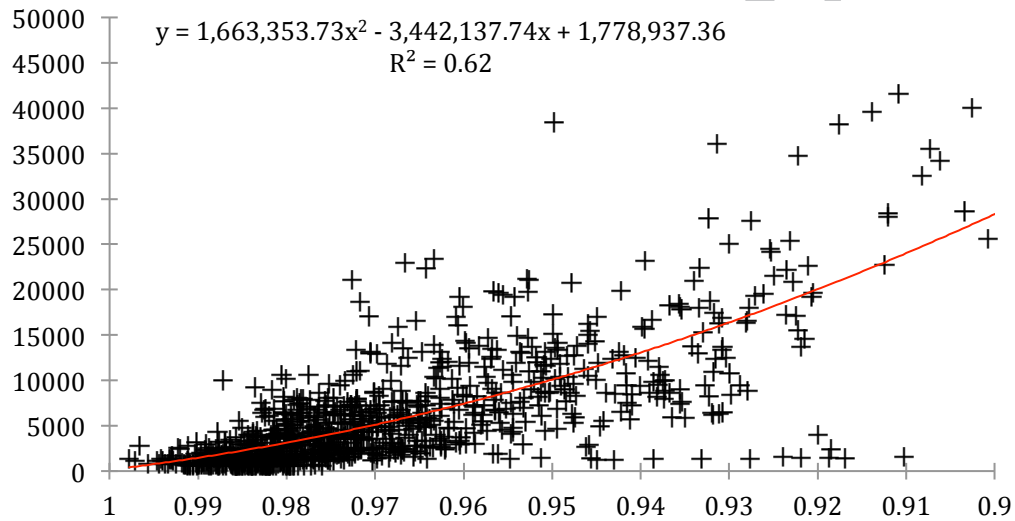
811 Orbital microwave sensors can monitor daily river discharge changes.
812 Calibration of remote sensing signal to discharge units is necessary.
813 Hydrological modeling is evaluated as a method to calibrate the remote
814 sensing.
815 Model-based calibration produces satisfactory results when compared to
816 ground-based information.
817 Independent river discharge information can now be obtained by use of
818 model-calibrated remote sensing.

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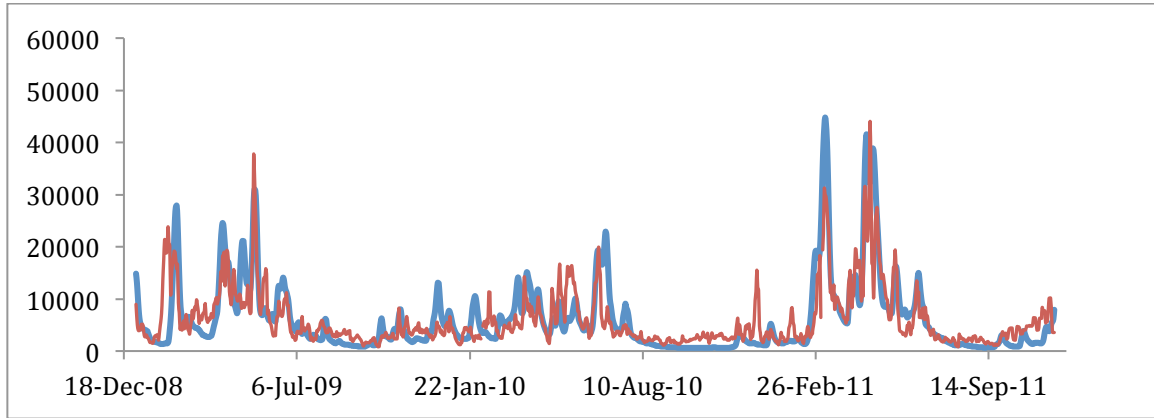




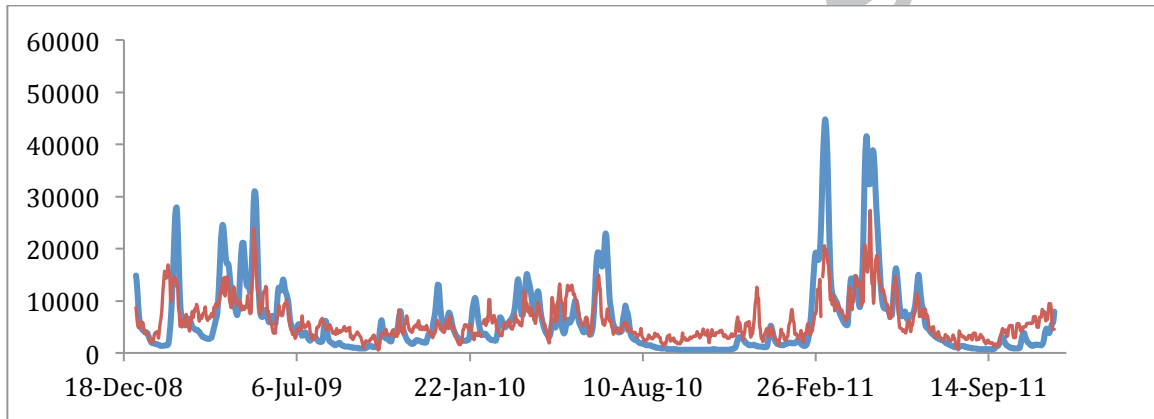
A



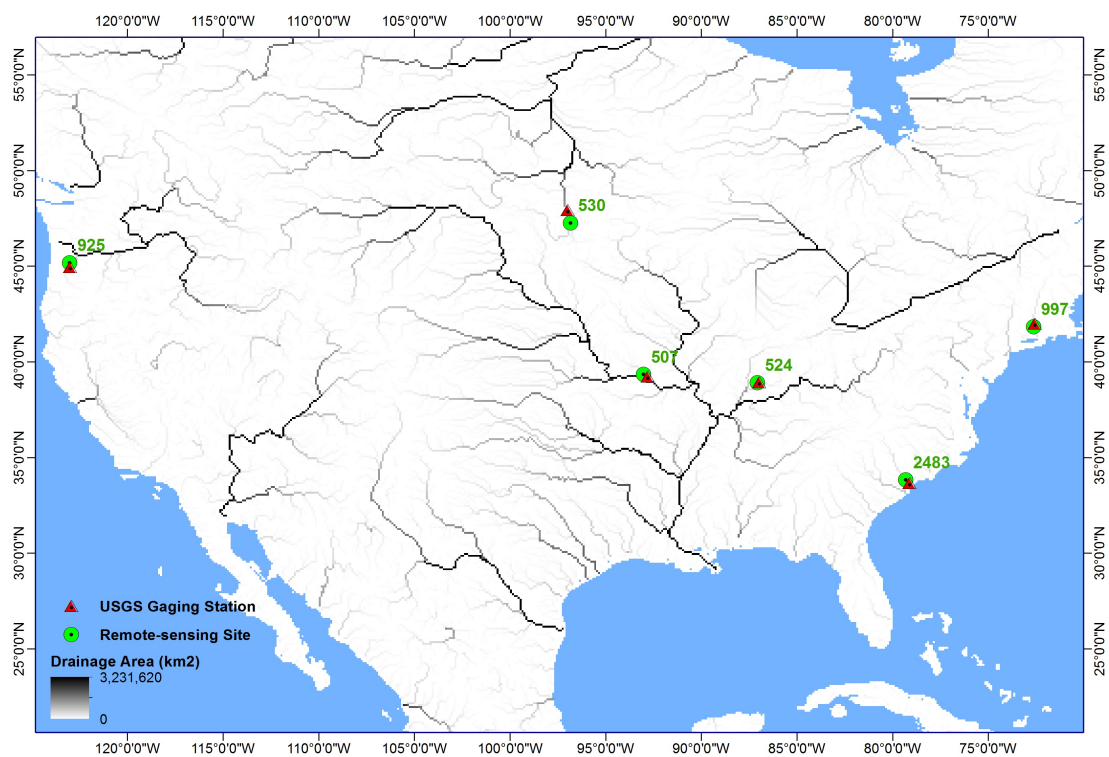
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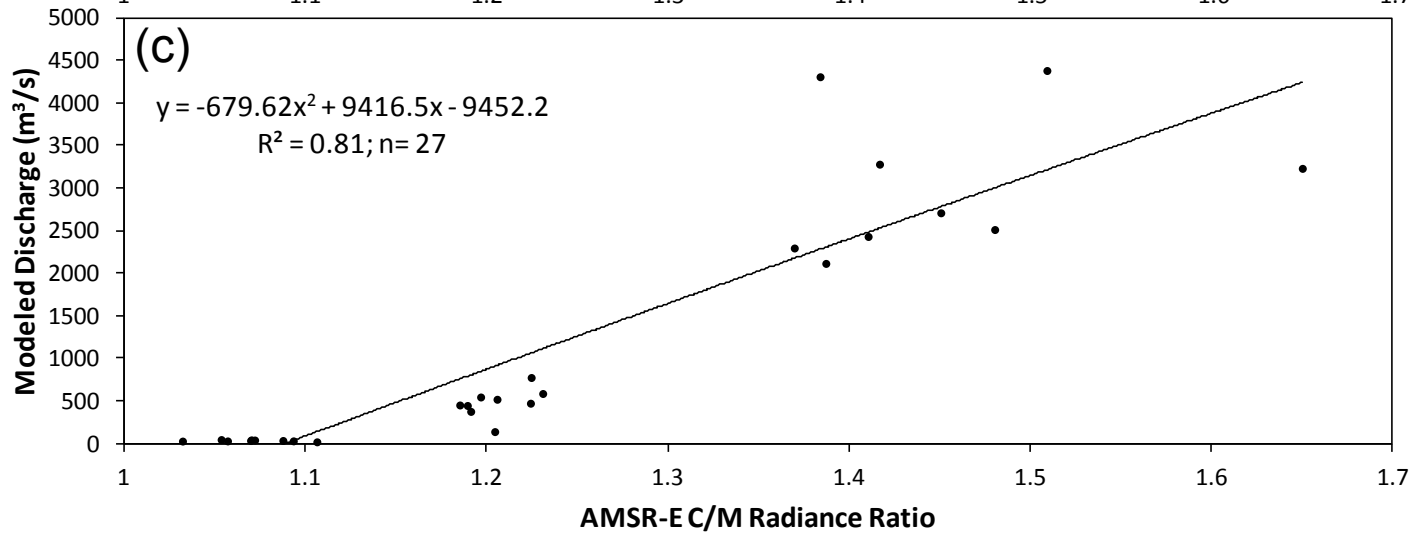
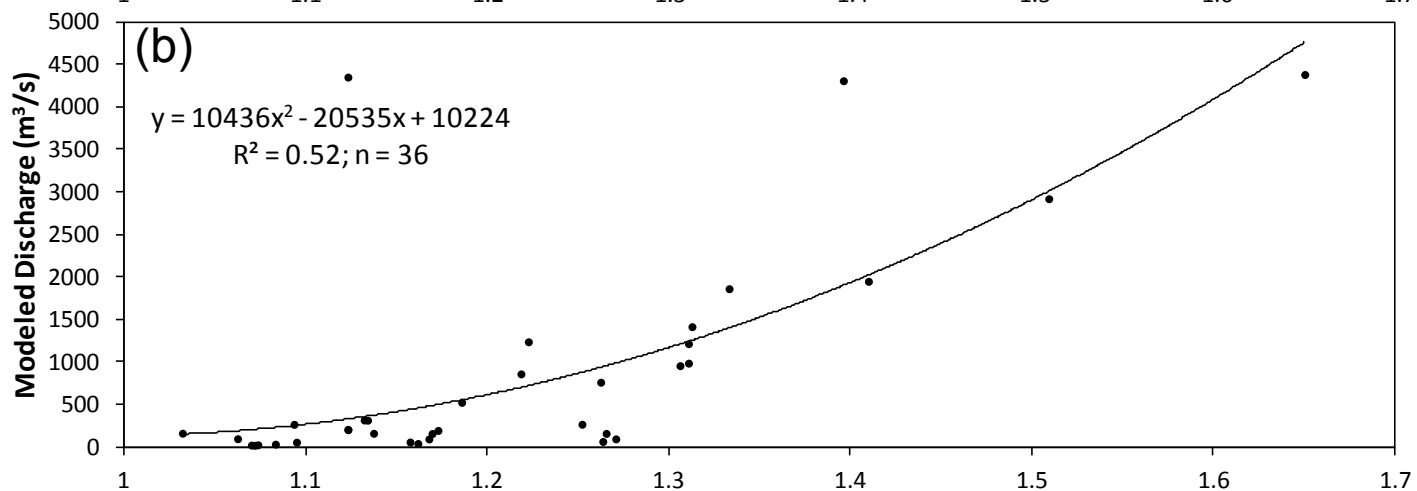
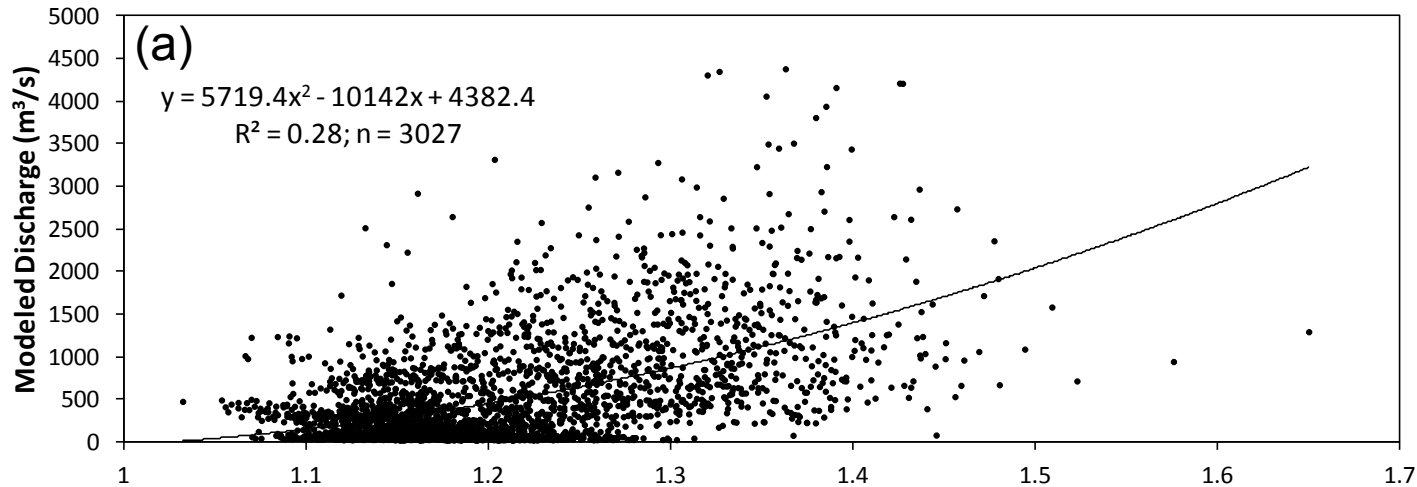


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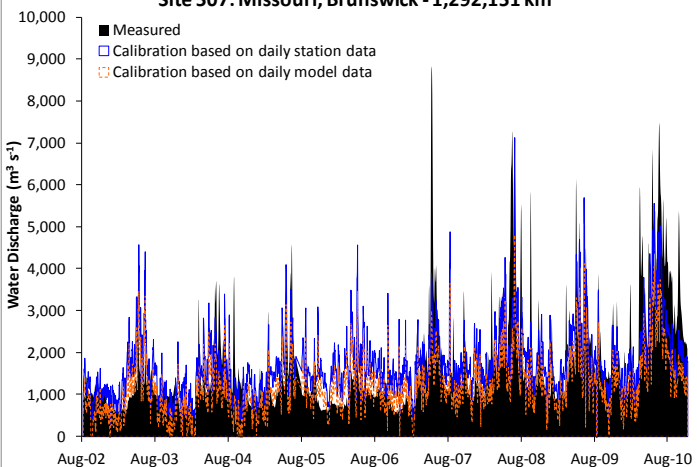


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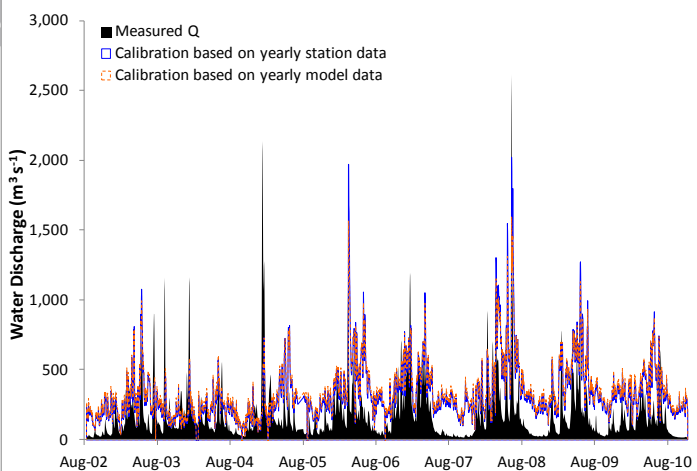
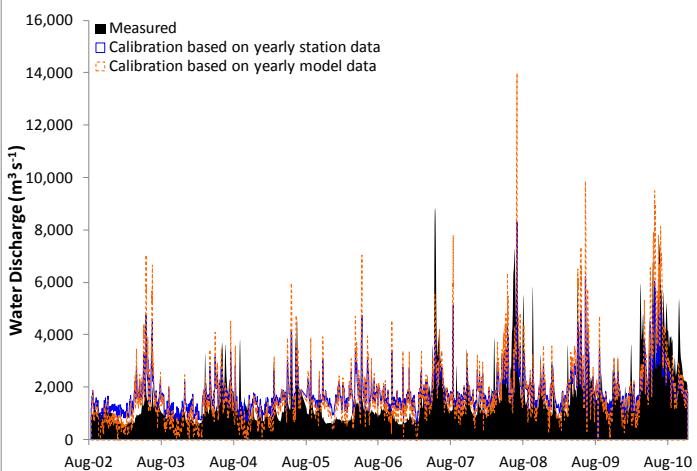
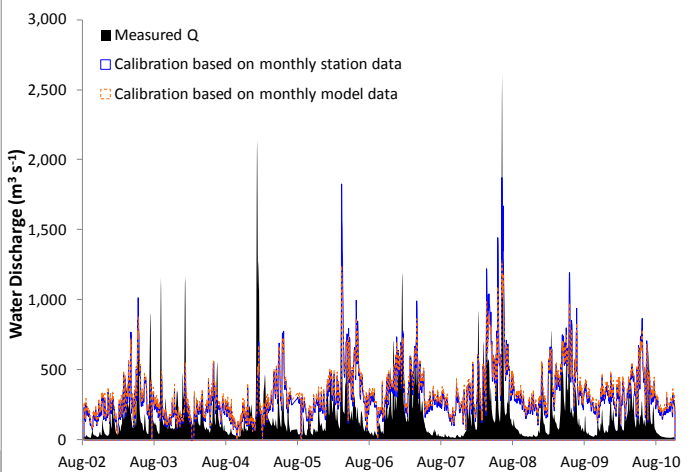
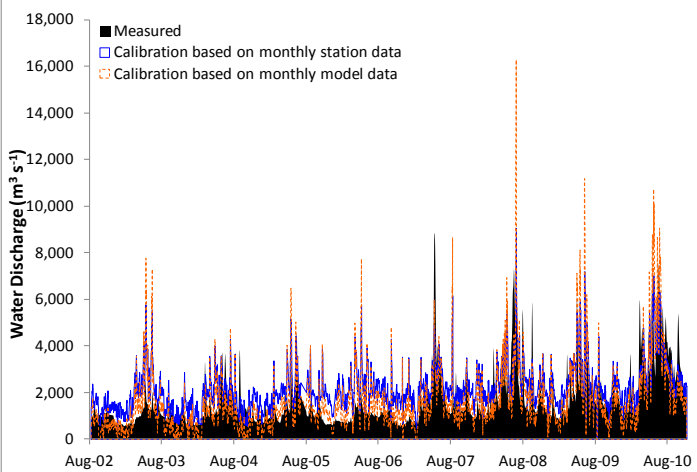
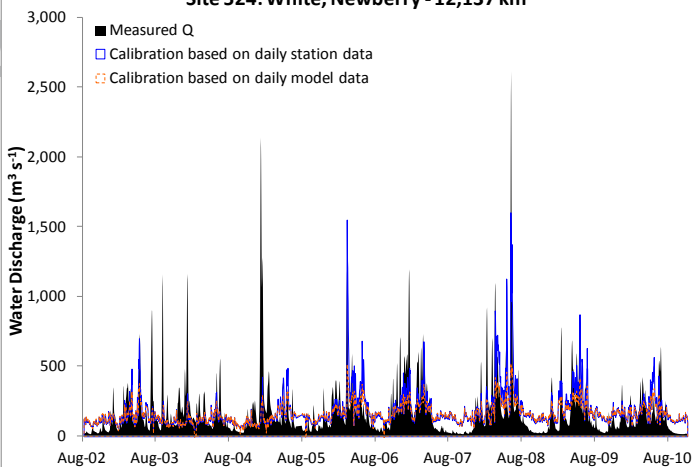




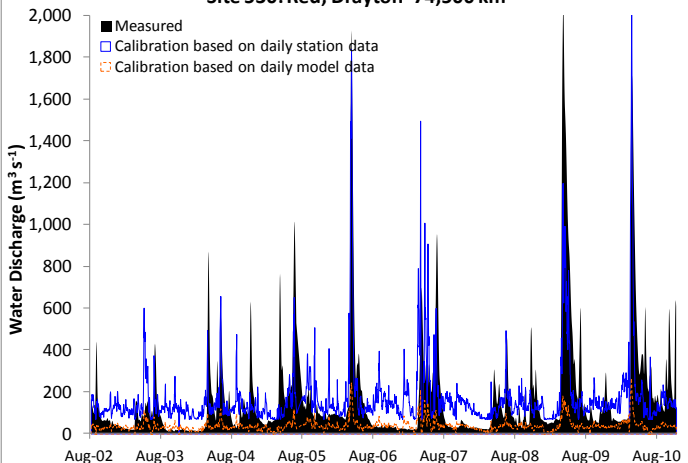
Site 507: Missouri, Brunswick - 1,292,151 km²



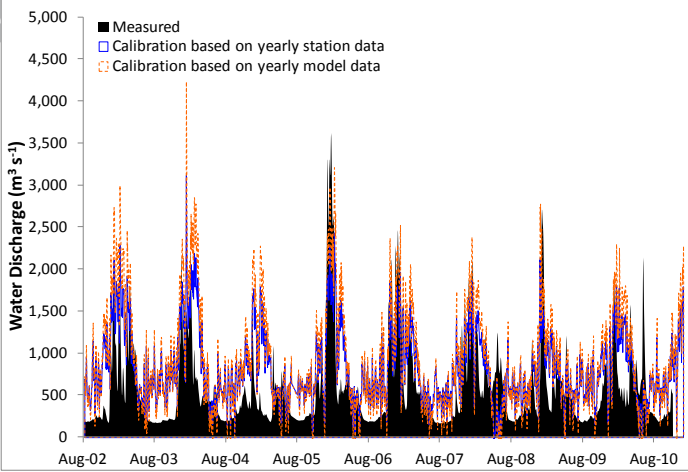
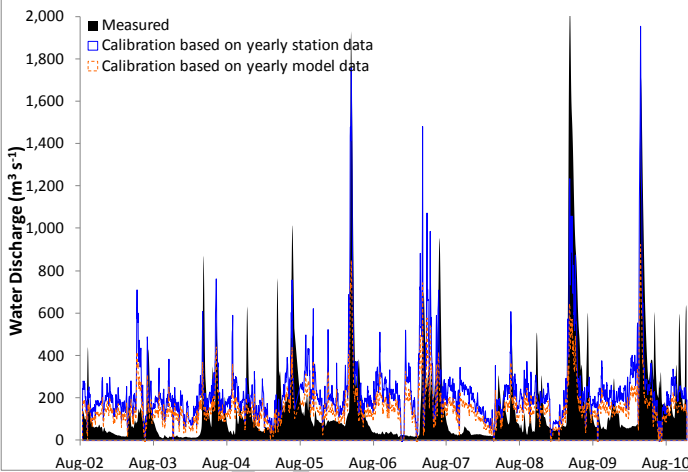
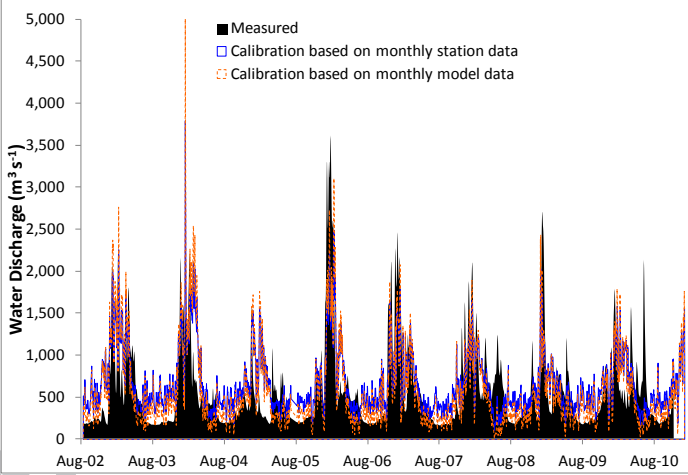
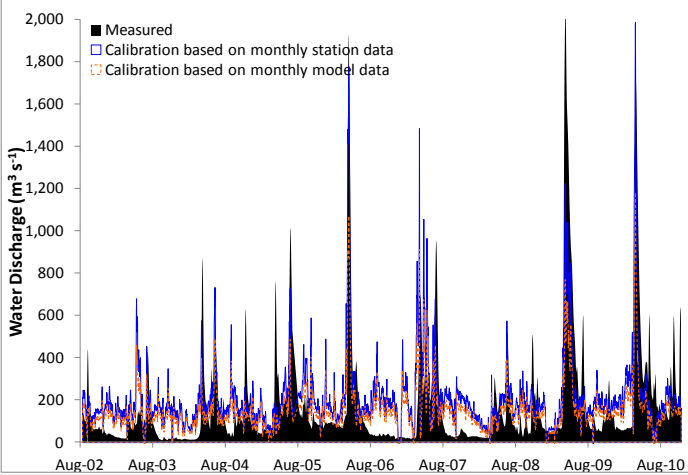
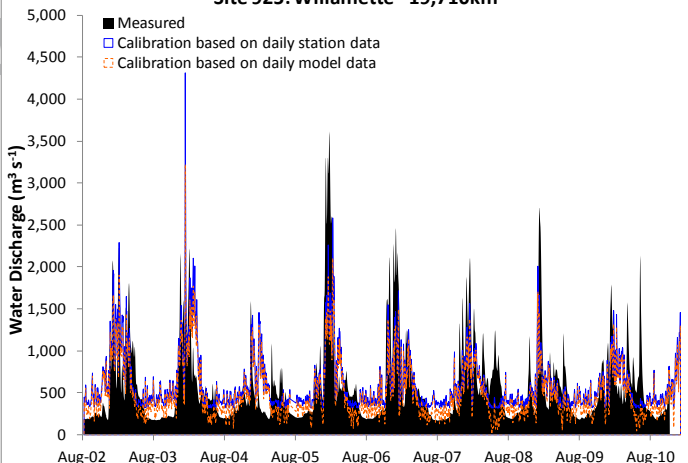
Site 524: White, Newberry - 12,137 km²



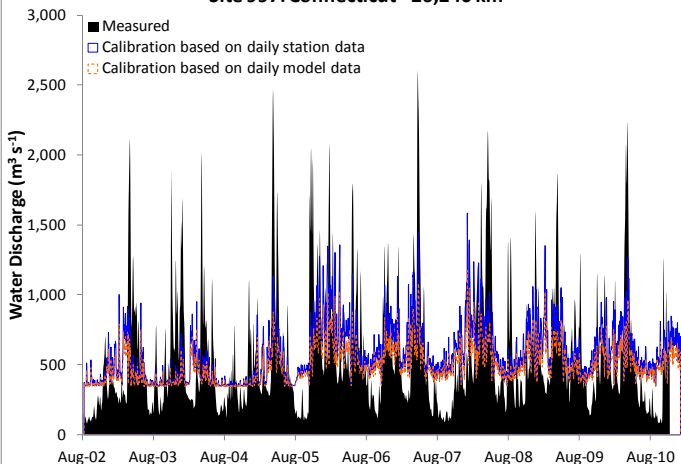
Site 530: Red, Drayton - 74,500 km²



Site 925: Willamette - 19,710km²



Site 997: Connecticut - 26,240 km²



Site 2483: Pee Dee- 28,706 km²

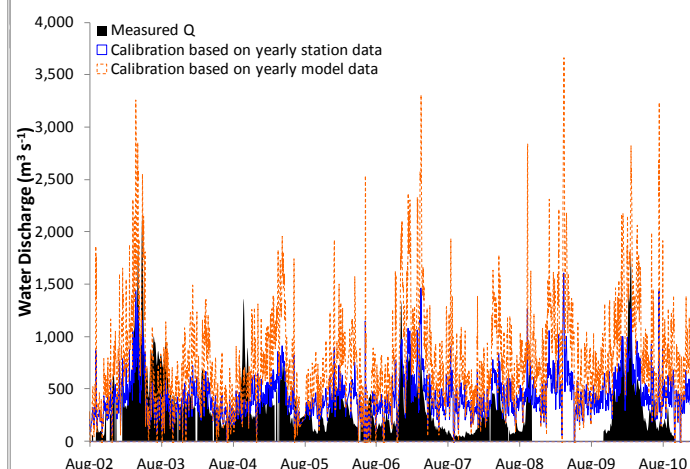
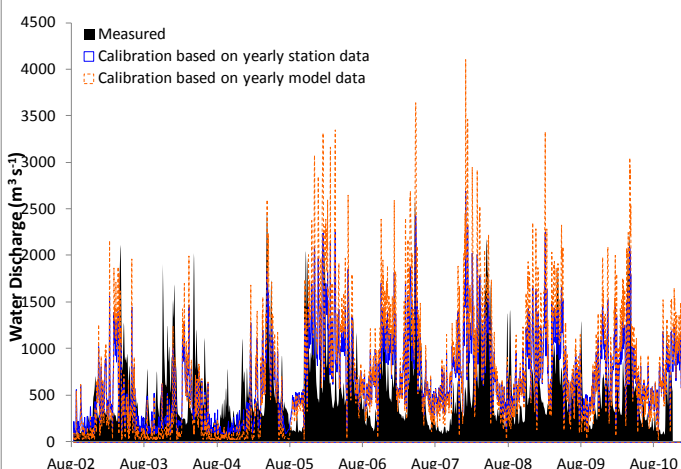
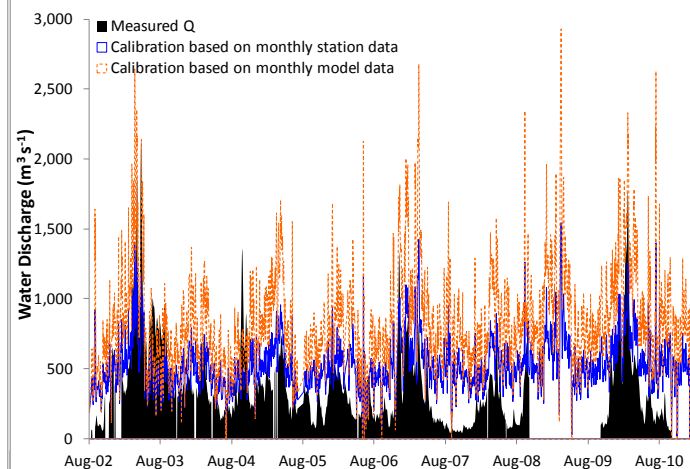
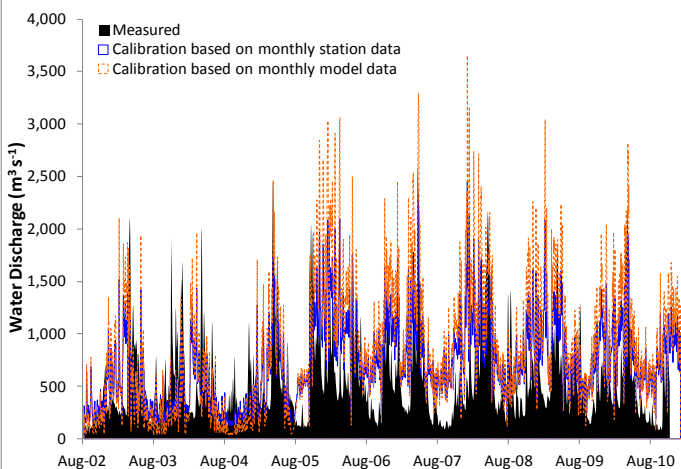
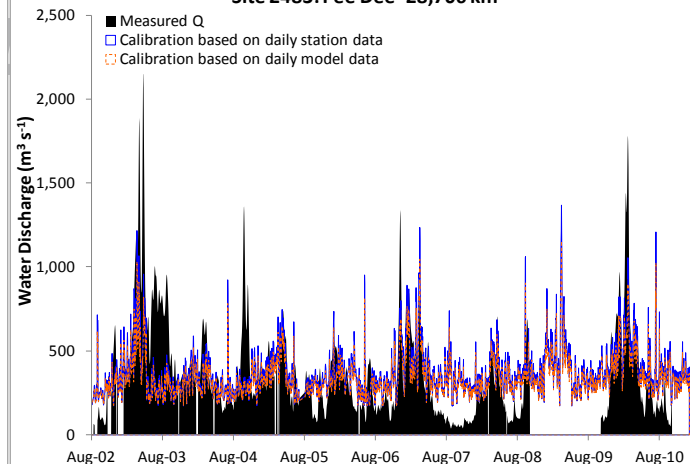
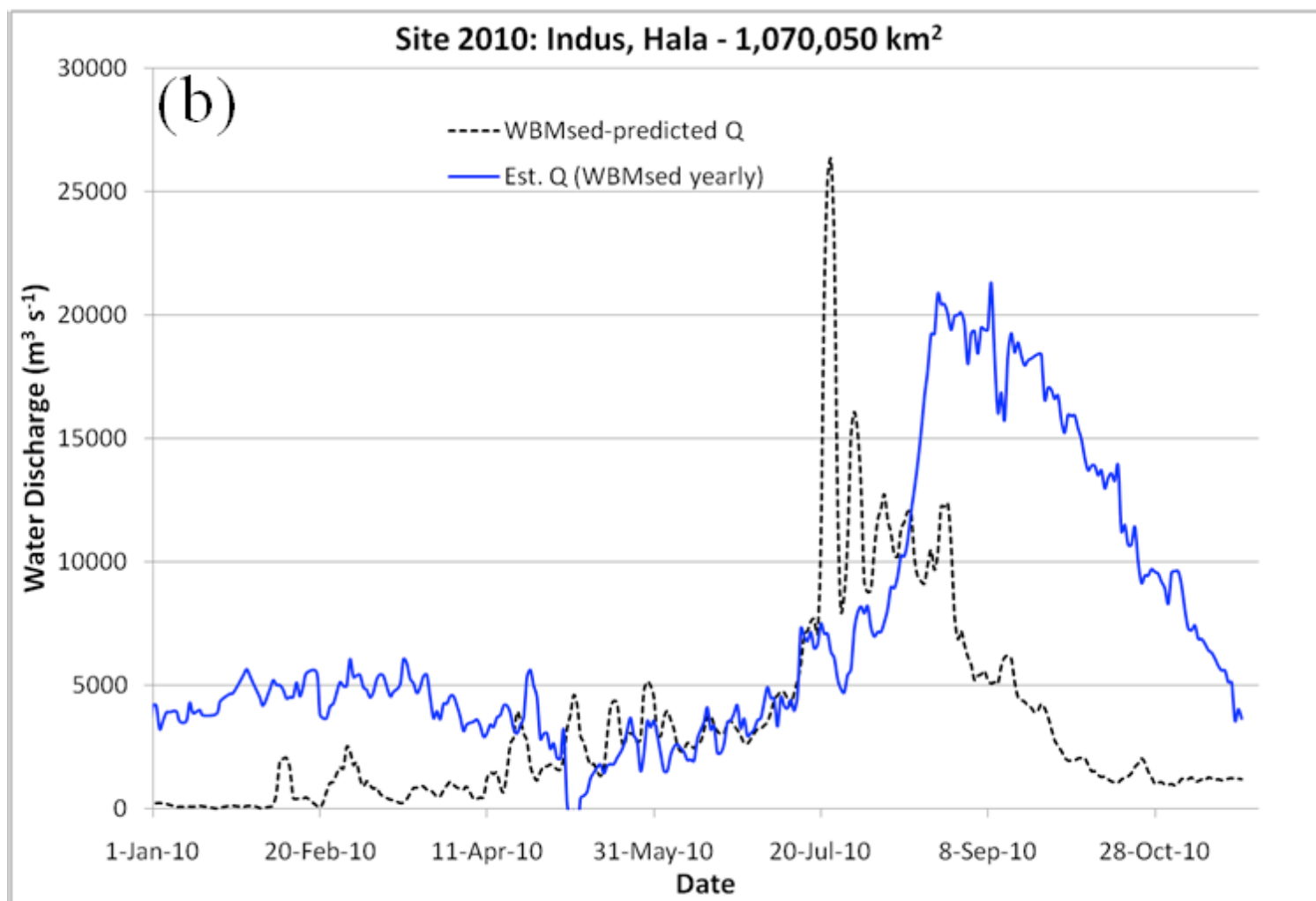


Figure 7



819 Table 1. Characteristics of 6 remote-sensing sites and corresponding USGS gaging stations (Figure 1) and the Indus site and gaging
 820 station (Figure 5). Site mean discharge is as predicted by WBM.

Site ID	Site River Name	Site Coordinates Lat/Long (dd)	Site Drainage Area (km ²)	Site Mean Discharge (m ³ /s)	Station ID	Station Coordinates Lat/Long (dd)	Station Drainage Area (km ²)	Station Mean Discharge (m ³ /s)
507	Missouri, Brunswick	39.34/-93.02	1,264,731	1206	06906500	39.22/-92.849	1,292,151	1709
524	White, Newberry	38.91/-87.07	12,802	161	03360500	38.92/-87.011	12,137	182
530	Red, Halstad	47.26/-96.84	65,000	39	05082500	47.92/-97.029	77,929	170
925	Willamette	45.18/-123.01	19,710	504	14191000	44.94/-123.042	18,928	591
997	Connecticut	41.84/-72.632	26,240	500	01184000	41.98/-72.606	25,116	567
2483	Pee Dee	33.82/-79.32	28,706	336	02135200	33.66/-79.155	36,660	372
2010	Indus, Hala	25.9/68.26	1,070,050	2730	Mandi Plain	31.75/74.75	20,886	497

821 Table 2. Rating curves equations of AMSR-E C/M radiance ratios versus WBM-predicted and gaging station-measured discharge with
 822 daily, monthly and yearly statistics (Figure 2). Site ID corresponds to Table 1 and Figures 1 and 5.
 823

ID	USGS daily	WBM daily	USGS monthly	WBM monthly	USGS yearly	WBM yearly
507	$530.71x^2 + 9092.7x - 9356.7$	$-4740.5x^2 + 20231x - 15676$	$1377.1x^2 + 9526.3x - 10485$	$25418x^2 - 42215x + 16604$	$7548.9x^2 - 8277.2x + 1349.9$	$18291x^2 - 26997x + 8637.6$
524	$1895.9x^2 - 3321.3x + 1503.2$	$-253.99x^2 + 1280.3x - 951.57$	$-559.11x^2 + 3004.7x - 2320.3$	$935.9x^2 - 344.86x - 481.06$	$1105.2x^2 - 625.27x - 371.88$	$-22.769x^2 + 1954.5x - 1816.6$
530	$4775.2x^2 - 8733.7x + 4062.1$	$248.38x^2 - 210.5x - 11.181$	$3413.6x^2 - 5463.7x + 2180.9$	$1514.8x^2 - 1969x - 555.27$	$3044.7x^2 - 4616.2x + 1729.7$	$665.89x^2 - 268.6x - 285.31$
925	$12268x^2 - 26478x + 14607$	$5719.4x^2 - 10142x + 4382.4$	$6893.6x^2 - 12527x + 5695.5$	$12063x^2 - 24172x + 12111$	$-996.07x^2 + 7989.8x - 7354.3$	$-679.62x^2 + 9416.5x - 9452.2$
997	$17051x^2 - 34488x + 17789$	$10897x^2 - 21890x + 11338$	$22195x^2 - 42451x + 20421$	$40085x^2 - 78585x + 38557$	$29201x^2 - 57348x + 28248$	$57460x^2 - 116560x + 59142$
2483	$21959x^2 - 41141x + 19441$	$17858x^2 - 33431x + 15821$	$17411x^2 - 29828x + 12726$	$38582x^2 - 67080x + 28870$	$18563x^2 - 32388x + 14093$	$46022x^2 - 80588x + 34948$